Lecture 9

Chemical Reaction Engineering (CRE) is the field that studies the rates and mechanisms of chemical reactions and the design of the reactors in which they take place.

Lecture 9 – Thursday 2/7/2013

Balances in terms of molar flow rates

Block 1: Mole Balances

Balance Equation on Every Species

Block 2: Rate Laws

Relative Rates

Transport Laws

- Block 3: Stoichiometry
- Block 4: Combine

Membrane Reactors:

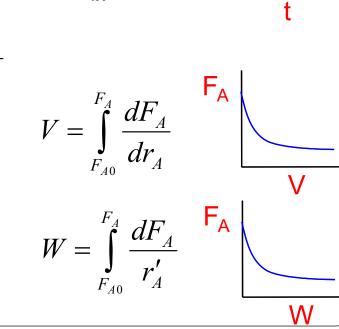
Used for thermodynamically limited reactions

Review Lecture 1

Reactor Mole Balances Summary

The GMBE applied to the four major reactor types (and the general reaction $A\rightarrow B$)

(and the general reaction A > b)			
Reactor	Differential	Algebraic	Integral
Batch	$\frac{dN_A}{dt} = r_A V$		$t = \int_{N_{A0}}^{N_A} \frac{dN_A}{r_A V}$
CSTR		$V = \frac{F_{A0} - F_{A}}{r}$	
PFR	$\frac{dF_A}{dr} - r$	$-r_A$	$V = \int_{\Gamma}^{F_A} \frac{dF_A}{dF_A}$



PBR

Mole Balance

① Write mole balance on each species,[†] $c.g., \quad \frac{dF_{A}}{dV} = r_{A}, \quad \frac{dF_{B}}{dV} = r_{B}, \quad \frac{dF_{C}}{dV} = r_{C}$

Rate Law

2) Write rate law in terms of concentration.

e.g.,
$$-r_{A} = k_{A} \left(C_{A} C_{B}^{2} - \frac{C_{C}}{K_{C}} \right)$$

Relative Rates

(3) Relate the rates of reaction of each species to one another.

$$\frac{-r_{A}}{1} = \frac{-r_{B}}{2} = \frac{r_{C}}{1}$$

e.g., $r_{B} = 2r_{A}$, $r_{C} = -r_{A}$

Stoichiometry

(a) Write the concentrations in terms of molar flow rates for isothermal gas-phase reactions.

e.g.,
$$C_{A} = C_{T0} \frac{F_{A}}{F_{T}} \frac{P}{P_{0}}$$
, $C_{B} = C_{T0} \frac{F_{B}}{F_{T}} \frac{P}{P_{0}}$
with $F_{T} = F_{A} + F_{B} + F_{C}$

(b) For liquid-phase reactions, use concentration, e.g., $C_{\rm A},\ C_{\rm B}$



Write the gas-phase pressure drop term in terms of molar flow rates.

$$\frac{dy}{dW} = -\frac{\alpha}{2y} \frac{F_{\rm T}}{F_{\rm T_0}}$$
, with $y = \frac{P}{P_0}$

Combine

Use an ODE solver or a nonlinear equation solver (e.g., Polymath) to combine Steps ① through ⑤ to solve for, for example, the profiles of molar flow rates, concentration, and pressure.

For PBR, use $\frac{dF_A}{dW} = r_A$, $\frac{dF_B}{dW} = r_B$, $\frac{dF_C}{dW} = r_C$.

Membrane reactors can be used to achieve conversions greater than the original equilibrium value. These higher conversions are the result of *Le Chatelier's principle*; you can remove the reaction products and drive the reaction to the right.

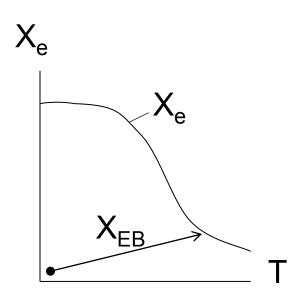
To accomplish this, a membrane that is permeable to that reaction product, but impermeable to all other species, is placed around the reacting mixture.

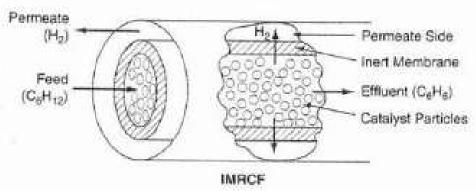
Dehydrogenation Reaction:

$$C_3H_8 \leftrightarrow H_2 + C_3H_6$$
 $A \leftrightarrow B + C$

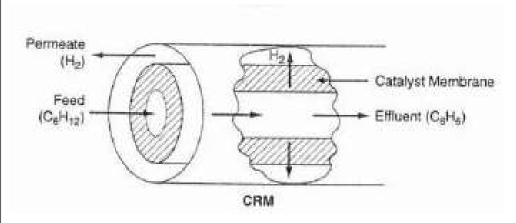
Thermodynamically Limited:

exothermic

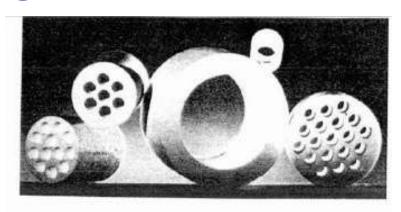




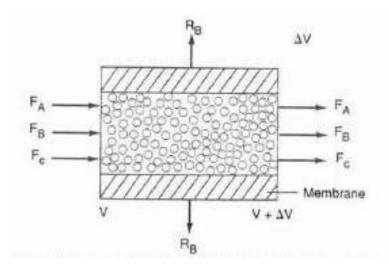
Cross section of IMRCF



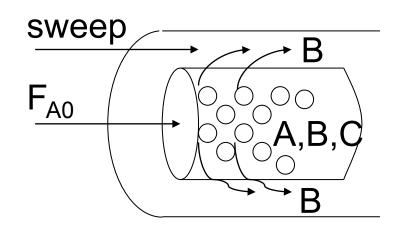
Cross section of CRM



Membrane Reactors



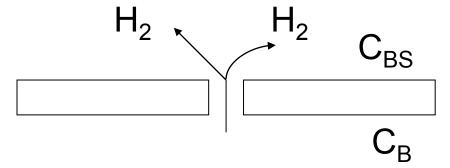
Schematic of IMRCF for mole balance



$$W = \rho_b V = solids \ weight$$

 $\rho_b = (1-\phi)\rho_C = bulk \ solids \ density$
 $\rho_C = density \ of \ solids$

$$\rho_b = \frac{volume\ solids}{volume\ total} * \frac{mass\ of\ solids}{volume\ solids}$$



A,C stay behind since they are too big

Mole Balance on Species A:

Species A:

$$In - out + generation = 0$$

$$F_A|_V - F_A|_{V + \Delta V} + r_A \Delta V = 0$$

$$\frac{dF_A}{dV} = r_A$$

Mole Balance on Species B:

Species B: In – out – out membrane + generation = 0

$$F_B|_V - F_B|_{V + \Lambda V} - R_B \Delta V + r_B \Delta V = 0$$

$$\frac{dF_B}{dV} = (r_B - R_B)$$

$$R_B = \frac{\text{moles of B through sides}}{\text{volume of reactor}}$$

$$W_B = k_C'(C_B - C_{BS}) = \frac{\text{molar flow rate through membrane}}{\text{surface area of membrane}} \left[\frac{mol}{m^2 \cdot s} \right]$$

$$a = \frac{\text{membrane surface area}}{\text{reactor volume}} = \frac{\pi DL}{\frac{\pi D^2}{4}L} = \frac{4}{D} \quad \left[\frac{m^2}{m^3}\right]$$

$$R_B = W_B a = k_C a \left[C_B - C_{BS} \right]$$

$$k_C = k_C' a$$

$$R_{B} = k_{C} \left[C_{B} - C_{BS} \right] \quad \left[\frac{mol}{m^{3} \cdot s} \right]$$

Neglected most of the time

Mole Balances:

$$(1) \quad \frac{dF_A}{dV} = r_A$$

$$(2) \quad \frac{dF_B}{dV} = r_B - R_B$$

(3)
$$\frac{dF_C}{dV} = r_C$$

Rate Law:

$$(4) \quad r_A = -k \left[C_A - \frac{C_B C_C}{K_C} \right]$$

Relative Rates:
$$\frac{-r_A}{1} = \frac{r_B}{1} = \frac{r_C}{1}$$

Net Rates: (5)
$$r_A = -r_B$$
, $r_A = -r_C$

Transport Law: (6)
$$R_B = k_C C_B$$

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Stoichiometry: (7)
$$C_A = C_{T0} \frac{F_A}{F_T}$$
 (isothermal, isobaric)

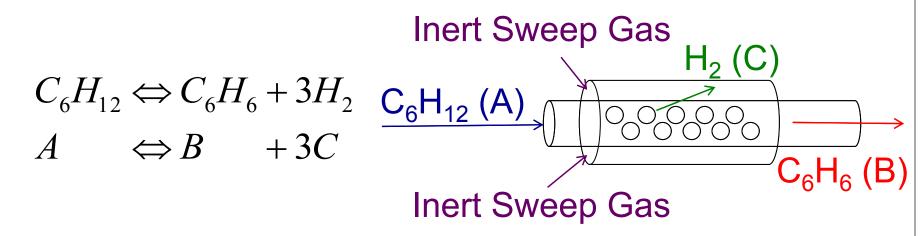
(8)
$$C_B = C_{T0} \frac{F_B}{F_T}$$

$$(9) \quad C_C = C_{T0} \frac{F_C}{F_T}$$

(10)
$$F_T = F_A + F_B + F_C$$

Parameters: $C_{TO} = 0.2$, $F_{AO} = 5$, k = 4, $K_C = 0.0004$, $k_C = 8$

Example: The following reaction is to be carried out isothermally in a membrane reactor with no pressure drop. The membrane is permeable to product C, but impermeable to all other species.



For membrane reactors, we cannot use conversion. We have to work in terms of the molar flow rates F_A , F_B , F_C .

Mole Balances

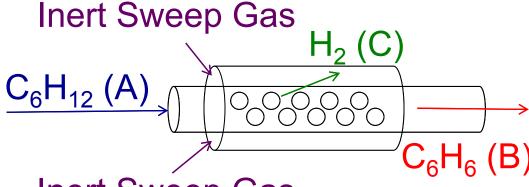
$$C_6H_{12} \Leftrightarrow C_6H_6 + 3H_2$$

 $A \Leftrightarrow B + 3C$

$$\frac{dF_A}{dW} = r_A'$$

$$\frac{dF_B}{dW} = r_B'$$

$$\frac{dF_C}{dW} = r_C' - k_C C_C$$



Inert Sweep Gas

Rate Law:

$$-r_A' = k_A \left| C_A - \frac{C_B C_C^3}{K_C} \right|$$

Relative Rates:

$$\frac{r_A'}{-1} = \frac{r_B'}{1} = \frac{r_C'}{3}$$

Net Rates:

$$r_B' = -r_A'$$

$$r_C' = -3r_A'$$

Stoichiometry:

Isothermal, no Pressure Drop

$$C_{T0} = \frac{P_0}{RT_0}$$

$$C_A = C_{T0} \frac{F_A}{F_T}$$

$$C_B = C_{T0} \frac{F_B}{F_T}$$

$$C_C = C_{T0} \frac{F_C}{F_T}$$

$$F_T = F_A + F_B + F_C$$

Combine: - Use Polymath

Parameters:
$$C_{T0} = 0.2 \frac{mol}{dm^3}$$

$$k_A = 10 \frac{dm^3}{kg \ cat \ s}$$

$$K_C = 200 \frac{mol^2}{dm^6}$$

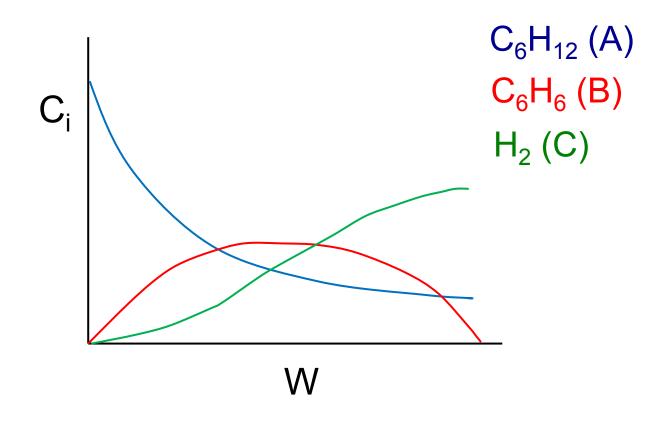
$$F_{A0} = 10 \frac{mol}{s}$$

$$C_{T0} = 0.2 \frac{mol}{dm^3}$$

$$F_{A0} = 10 \frac{mol}{s}$$

$$k_A = 10 \frac{dm^3}{kg \ cat \ s}$$

$$k_C = 0.5 \frac{dm^3}{kg \ cat \ s}$$



End of Lecture 9