

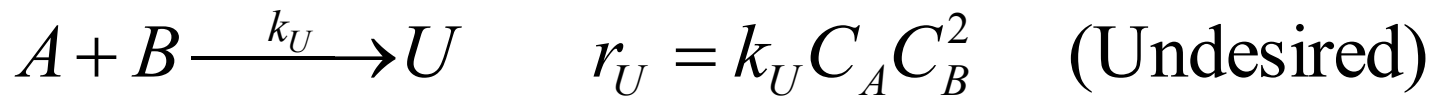
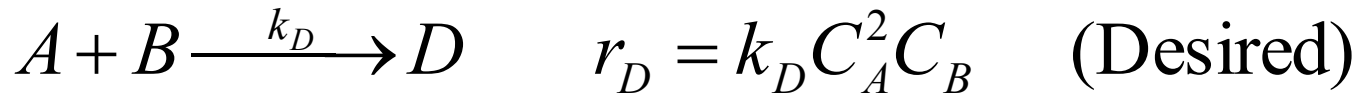
Lecture 10

Chemical Reaction Engineering (CRE) is the field that studies the rates and mechanisms of chemical reactions and the design of the reactors in which they take place.

Lecture 10 – Tuesday 2/12/2013

- Block 1: **Mole Balances**
 - Block 2: **Rate Laws**
 - Block 3: **Stoichiometry**
 - Block 4: **Combine**
-
- Definition of Selectivity
 - **Semibatch Reactors**

Selectivity in Multiple Reactions



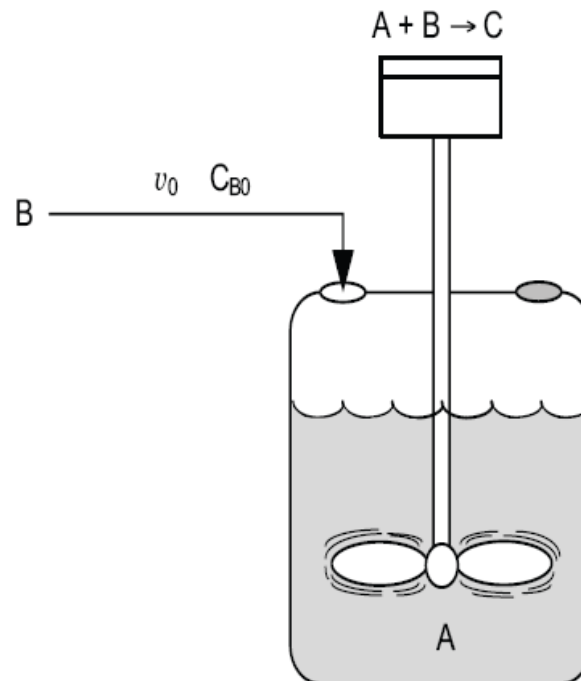
| | Selectivity | Yield |
|---------------|-----------------------------|------------------------------------|
| Instantaneous | $S_{D/U} = r_D / r_U$ | $Y_D = r_D / -r_A$ |
| Overall | $\hat{S}_{D/U} = F_D / F_U$ | $\hat{Y}_D = F_D / (F_{A0} - F_A)$ |

$$S_{D/U} = \frac{r_D}{r_U} = \frac{k_D C_A^2 C_B}{k_U C_A C_B^2} = \frac{k_D C_A}{k_U C_B}$$

Keep C_A high and C_B low.

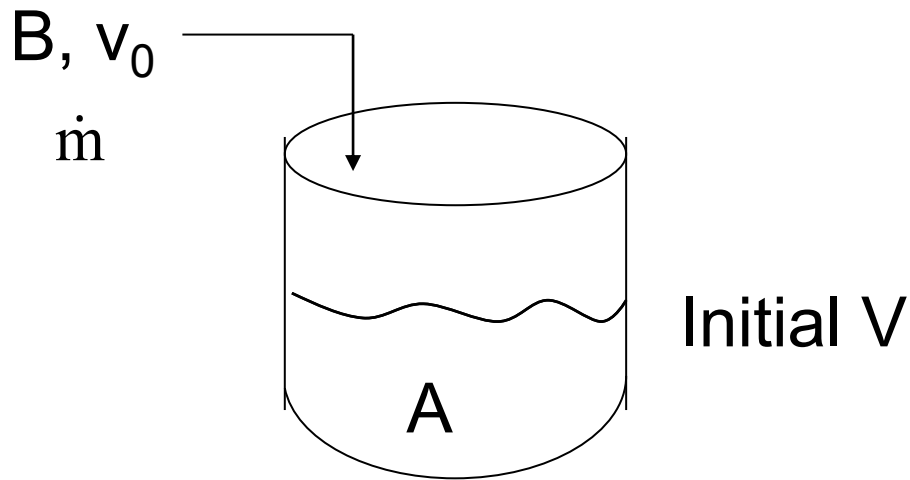
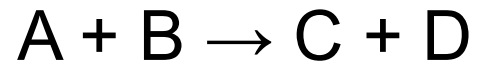
Semibatch Reactors

- Semibatch reactors can be very effective in maximizing selectivity in liquid phase reactions.
- The reactant that starts in the reactor is always the limiting reactant.



Semibatch Reactors

Semibatch reactors



Liquid level and volume increase

Semibatch Reactors

1) Mass Balance: $\frac{dm}{dt} = \dot{m}$

$$\dot{m} = v_0 \rho_0 \quad \text{and} \quad m = V \rho_0$$

$$\frac{dm}{dt} = \rho_0 \frac{dV}{dt} = \rho_0 v_0$$

$$\frac{dV}{dt} = v_0$$

$$t = 0 \quad V = V_0$$

$$V = V_0 + v_0 t$$

Semibatch Reactors

1) Mole Balance on Species A:

$$[\text{in}] - [\text{out}] + [\text{gen}] = [\text{acc}]$$

$$0 - 0 + r_A V = \frac{dN_A}{dt}$$

$$\frac{dN_A}{dt} = \frac{d[C_A V]}{dt} = V \frac{dC_A}{dt} + C_A \frac{dV}{dt}$$

$$\frac{dV}{dt} = v_0$$

$$\frac{dC_A}{dt} = r_A - \frac{v_0 C_A}{V}$$

Semibatch Reactors

1) Mole Balance on Species B:

$$F_{B0} - 0 + r_B V = \frac{dN_B}{dt}$$

$$\frac{dN_B}{dt} = \frac{d[C_B V]}{dt} = V \frac{dC_B}{dt} + C_B \frac{dV}{dt}$$

$$F_{B0} = C_{B0} \nu_0 \quad \frac{dV}{dt} = \nu_0$$

$$\frac{dC_B}{dt} = r_B + \frac{(C_{B0} - C_B) \nu_0}{V}$$

Semibatch Reactors

1) Mass and Mole Balance Summary

$$(1) \quad \frac{dC_A}{dt} = r_A - \frac{\nu_0 C_A}{V}$$

$$(2) \quad \frac{dC_B}{dt} = r_B - \frac{\nu_0 (C_{B0} - C_B)}{V}$$

$$(3) \quad \frac{dC_C}{dt} = r_C - \frac{\nu_0 C_C}{V}$$

$$(4) \quad \frac{dC_D}{dt} = r_D - \frac{\nu_0 C_D}{V}$$

$$(5) \quad V = V_0 + \nu_0 t$$

Semibatch Reactors

2) Rate Laws

$$(6) \quad r_A = kC_A C_B$$

3) Stoichiometry

$$\frac{-r_A}{1} = \frac{-r_B}{1} = \frac{r_C}{1} = \frac{r_D}{1}$$

$$(7) \quad r_B = r_A$$

$$(8) \quad r_C = -r_A$$

$$(9) \quad r_D = -r_A$$

$$(10) \quad X = \frac{N_{A0} - N_A}{N_{A0}}$$

$$(11) \quad N_{A0} = C_{A0} V_0$$

$$(12) \quad N_A = C_A V$$

4) Parameters

$$C_{A0}, V_0, \nu_0, k, C_{B0}$$

Semibatch Reactors

POLYMATH Report
Ordinary Differential Equations

Calculated values of DEQ variables

| | Variable | Initial value | Minimal value | Maximal value | Final value |
|----|----------|---------------|---------------|---------------|-------------|
| 1 | Ca | 0.05 | 7.731E-06 | 0.05 | 7.731E-06 |
| 2 | Cao | 0.05 | 0.05 | 0.05 | 0.05 |
| 3 | Cb | 0 | 0 | 0.0125077 | 0.0125077 |
| 4 | Cbo | 0.025 | 0.025 | 0.025 | 0.025 |
| 5 | Cc | 0 | 0 | 0.0121468 | 0.0083256 |
| 6 | Cd | 0 | 0 | 0.0121468 | 0.0083256 |
| 7 | k | 2.2 | 2.2 | 2.2 | 2.2 |
| 8 | ra | 0 | -0.0001644 | 0 | -2.127E-07 |
| 9 | rate | 0 | 0 | 0.0001644 | 2.127E-07 |
| 10 | t | 0 | 0 | 500. | 500. |
| 11 | V | 5. | 5. | 30. | 30. |
| 12 | vo | 0.05 | 0.05 | 0.05 | 0.05 |
| 13 | Vo | 5. | 5. | 5. | 5. |
| 14 | X | 0 | 0 | 0.9990722 | 0.9990722 |

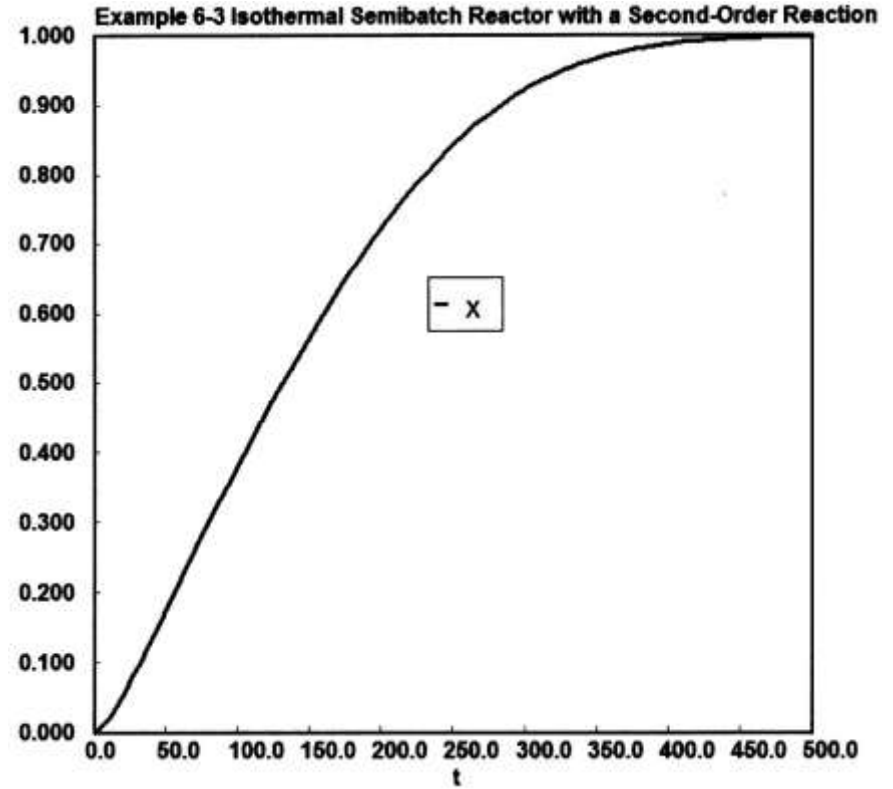
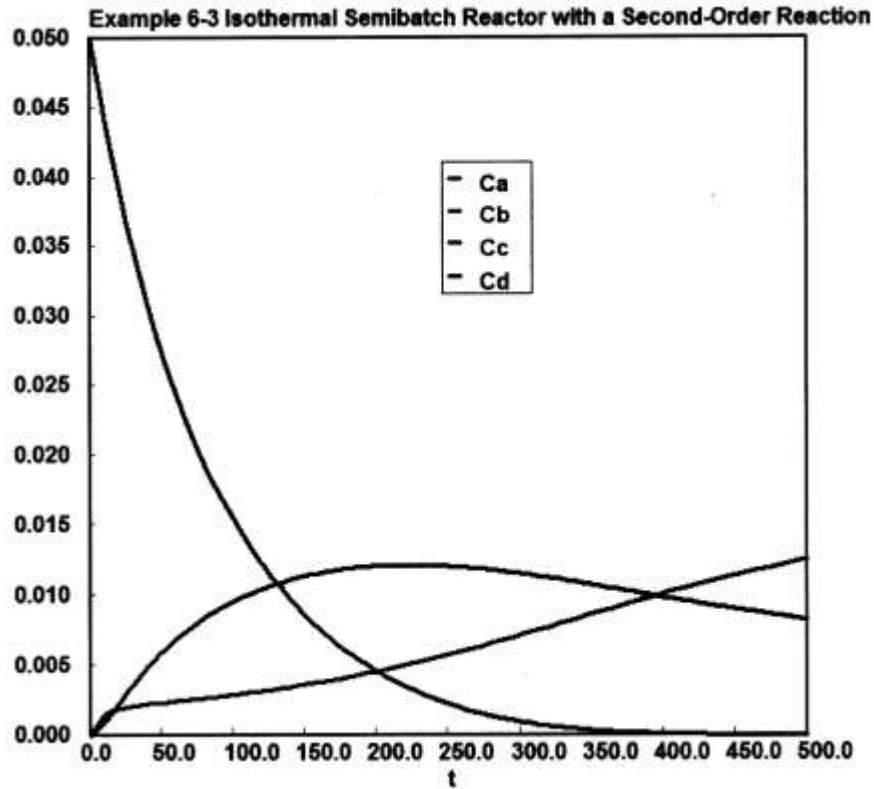
Differential equations

- 1 $d(Ca)/d(t) = ra - vo * Ca / V$
- 2 $d(Cb)/d(t) = ra + (Cbo - Cb) * vo / V$
- 3 $d(Cc)/d(t) = -ra - vo * Cc / V$
- 4 $d(Cd)/d(t) = -ra - vo * Cd / V$

Explicit equations

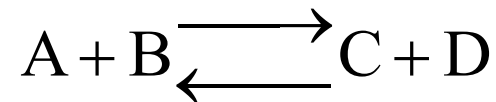
- 1 $vo = 0.05$
- 2 $Vo = 5$
- 3 $V = Vo + vo * t$
- 4 $k = 2.2$
- 5 $Cbo = 0.025$
- 6 $ra = -k * Ca * Cb$
- 7 $Cao = 0.05$
- 8 $rate = -ra$
- 9 $X = (Cao * Vo - Ca * V) / (Cao * Vo)$

Semibatch Reactors



Equilibrium Conversion in Semibatch Reactors with Reversible Reactions

Consider the following reaction:



Everything is the same as for the irreversible case, except for the rate law:

$$-r_A = k_A \left[C_A C_B - \frac{C_C C_D}{K_C} \right]$$

Equilibrium Conversion in Semibatch Reactors with Reversible Reactions

Where:

$$C_A = \frac{N_{A0}(1-X)}{V}$$
$$C_B = \frac{(F_{B0}t - N_{A0}X)}{V}$$
$$C_C = C_D = \frac{N_{A0}X}{V}$$

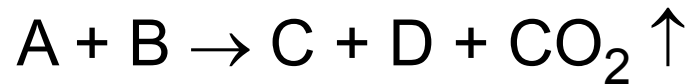
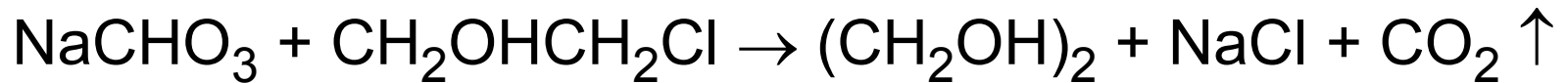
At equilibrium, $-r_A = 0$ then

$$K_C = \frac{C_{Ce}C_{De}}{C_{Ae}C_{Be}} = \frac{N_{Ce}N_{De}}{N_{Ae}N_{Be}} = \frac{N_{A0}X_e^2}{(1-X_e)(F_{B0}t - N_{A0}X_e)}$$

X_e changes with time.

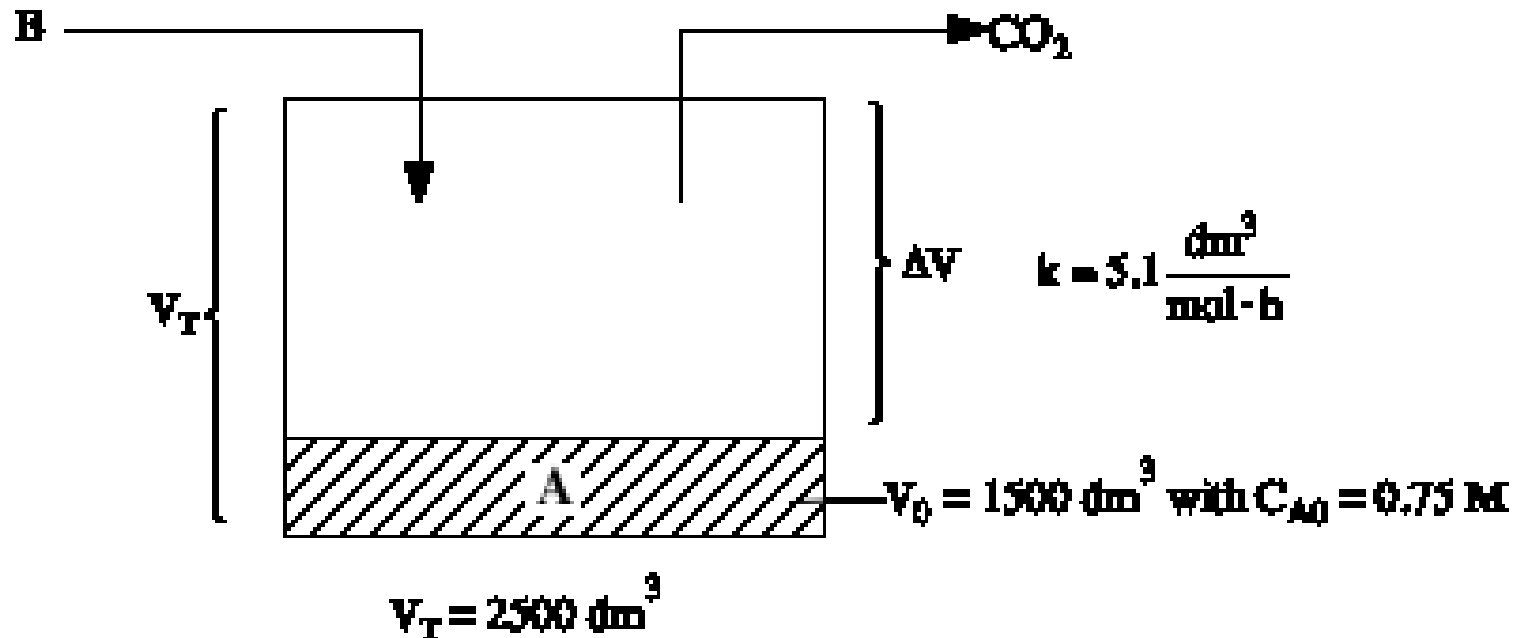
P6-6_B - Semibatch Reactors

Sodium Bicarbonate + Ethylene Chlorohydrin \rightarrow Ethylene Glycol + NaCl + CO₂↑



$$F_{B0} = 0.1 \frac{\text{mol}}{\text{min}}$$

$$C_{B0} = 1.5 \text{ M}$$



P6-6_B - Semibatch Reactors

Semibatch Reactors in terms of **Moles**



Mole Balances

$$A \quad (1) \quad \frac{dN_a}{dt} = r_A V$$

$$B \quad (2) \quad \frac{dN_b}{dt} = F_{B0} + r_B V$$

$$C \quad (3) \quad \frac{dN_c}{dt} = r_C V$$

$$D \quad (4) \quad N_D = N_C$$

$$CO_2 \quad 0 = -F_{CO_2} + r_{CO_2} V$$

$$(5) \quad F_{CO_2} = r_{CO_2} V$$

$$(6) \quad \frac{dV}{dt} = v_0 - v_{CO_2}$$

$$(7) \quad v_{CO_2} = \frac{F_{CO_2} MW_{CO_2}}{RHO}$$

$$(8) \quad MW = 44$$

$$(9) \quad RHO = 1000$$

$$(10) \quad C_a = N_A/V$$

$$(11) \quad C_B = N_B/V$$

$$(12) \quad r_A = -kC_A C_B$$

$$(13) \quad X = \frac{N_{a0} - N_a}{N_{a0}}$$

$$(14) \quad N_{a0} = V_0 C_{a0}$$

Rate Laws

Rest of the Polymath Statements
Similar to Concentration Program

P6-6 Semibatch: Moles, N_a , N_b , etc.

POLYMATH Report

Ordinary Differential Equations

Calculated values of DEQ variables

| | Variable | Initial value | Minimal value | Maximal value | Final value |
|----|----------|---------------|---------------|---------------|-------------|
| 1 | Ca | 0.75 | 8.845E-14 | 0.75 | 8.845E-14 |
| 2 | Cao | 0.75 | 0.75 | 0.75 | 0.75 |
| 3 | Cb | 0 | 0 | 0.15303 | 0.15303 |
| 4 | Cbo | 1.5 | 1.5 | 1.5 | 1.5 |
| 5 | Cc | 0 | 0 | 0.4967829 | 0.45909 |
| 6 | Cd | 0 | 0 | 0.4967829 | 0.45909 |
| 7 | Fbo | 6. | 6. | 6. | 6. |
| 8 | FCO2 | 0 | 0 | 5.987114 | 1.692E-10 |
| 9 | k | 5.1 | 5.1 | 5.1 | 5.1 |
| 10 | MWCO2 | 44. | 44. | 44. | 44. |
| 11 | Na | 1125. | 2.167E-10 | 1125. | 2.167E-10 |
| 12 | Nao | 1125. | 1125. | 1125. | 1125. |
| 13 | Nb | 0 | 0 | 375. | 375. |
| 14 | Nc | 0 | 0 | 1125. | 1125. |
| 15 | ra | 0 | -0.0039389 | 0 | -6.903E-14 |
| 16 | rho | 1000. | 1000. | 1000. | 1000. |
| 17 | t | 0 | 0 | 250. | 250. |
| 18 | V | 1500. | 1500. | 2450.5 | 2450.5 |
| 19 | vCO2 | 0 | 0 | 0.263433 | 7.443E-12 |
| 20 | vo | 4. | 4. | 4. | 4. |
| 21 | X | 0 | 0 | 1. | 1. |

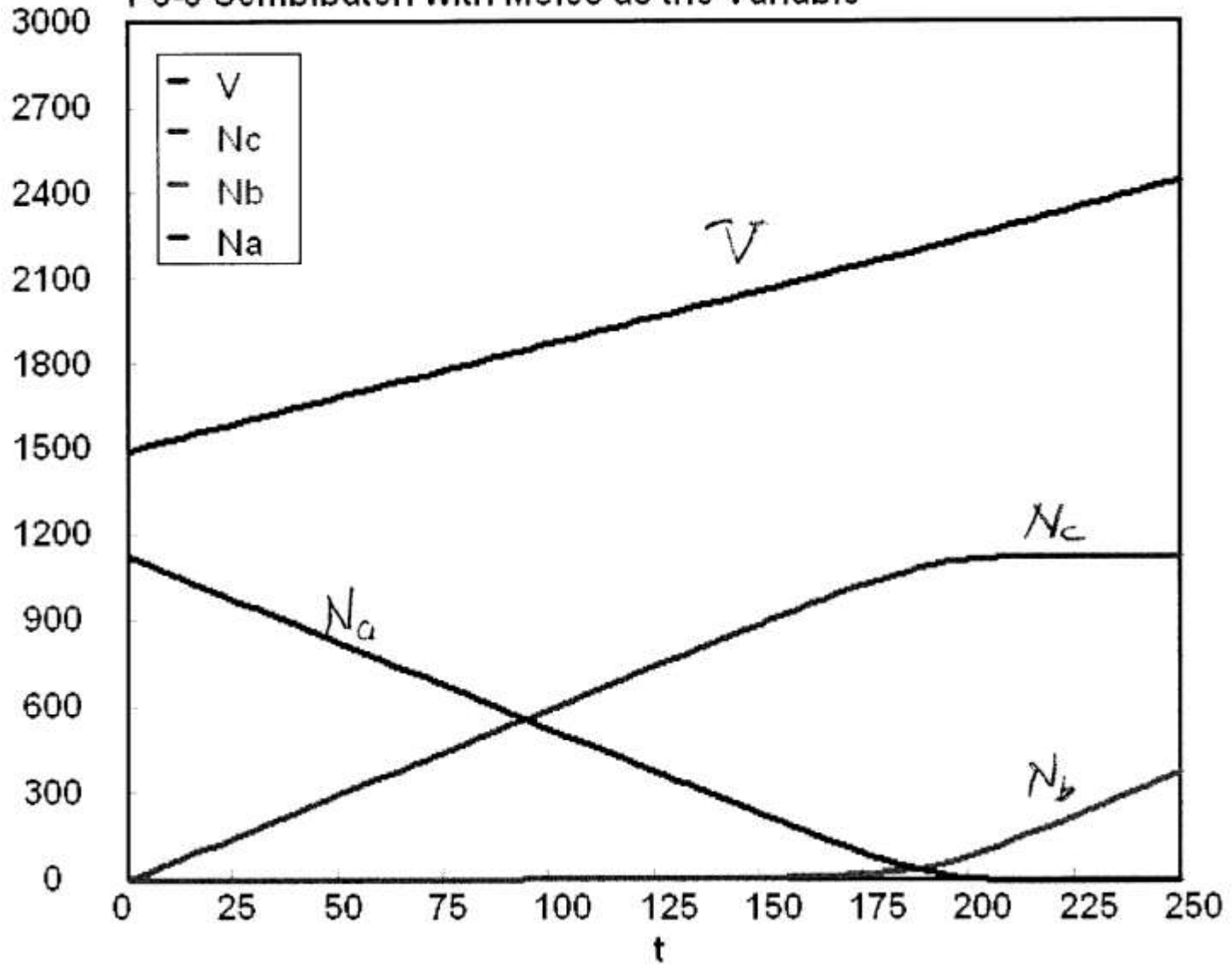
Differential equations

- 1 $d(V)/d(t) = v_o - v_{CO2}$
- 2 $d(N_c)/d(t) = -r_a * V$
- 3 $d(N_b)/d(t) = F_{b0} + r_a * V$
- 4 $d(N_a)/d(t) = r_a * V$

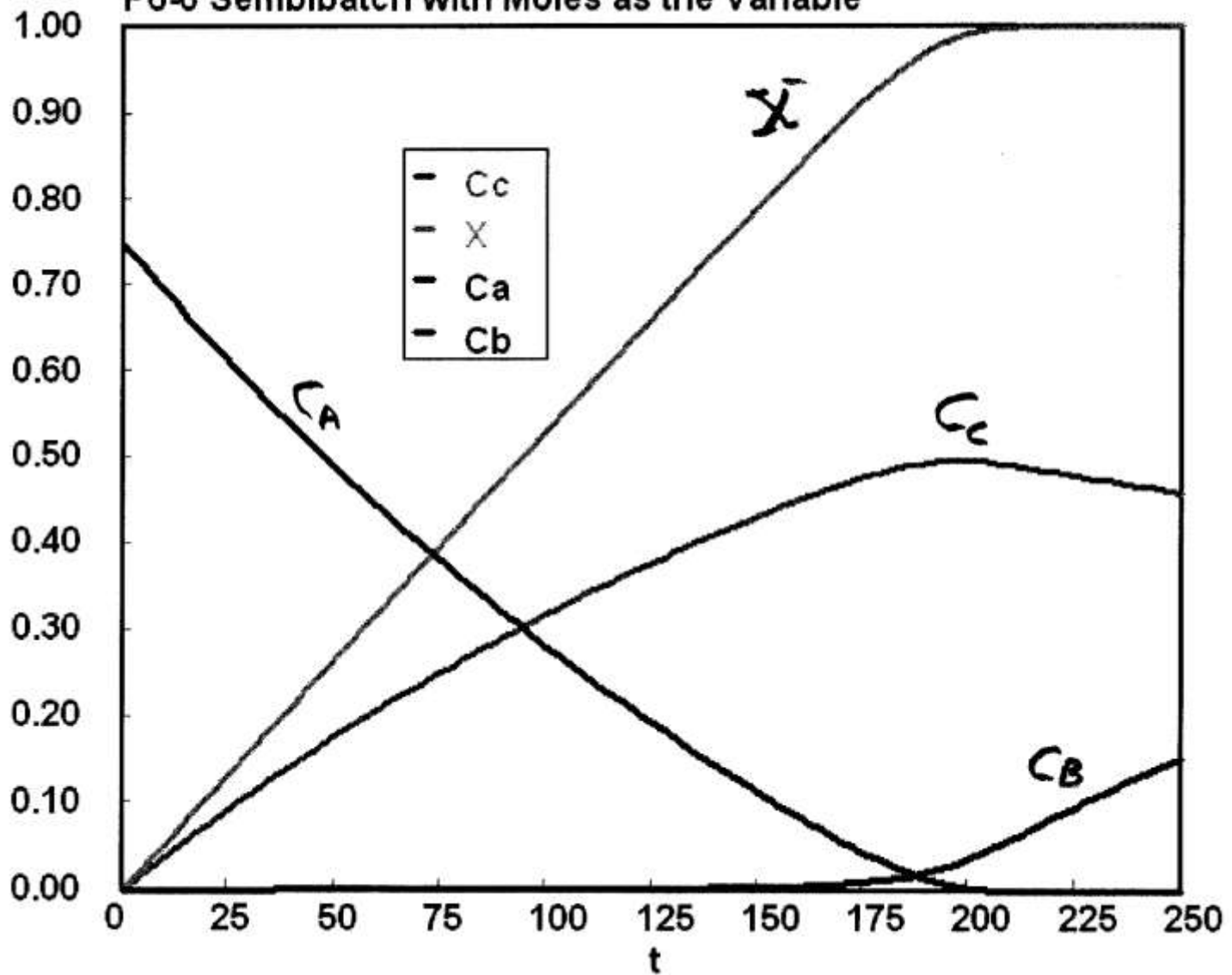
Explicit equations

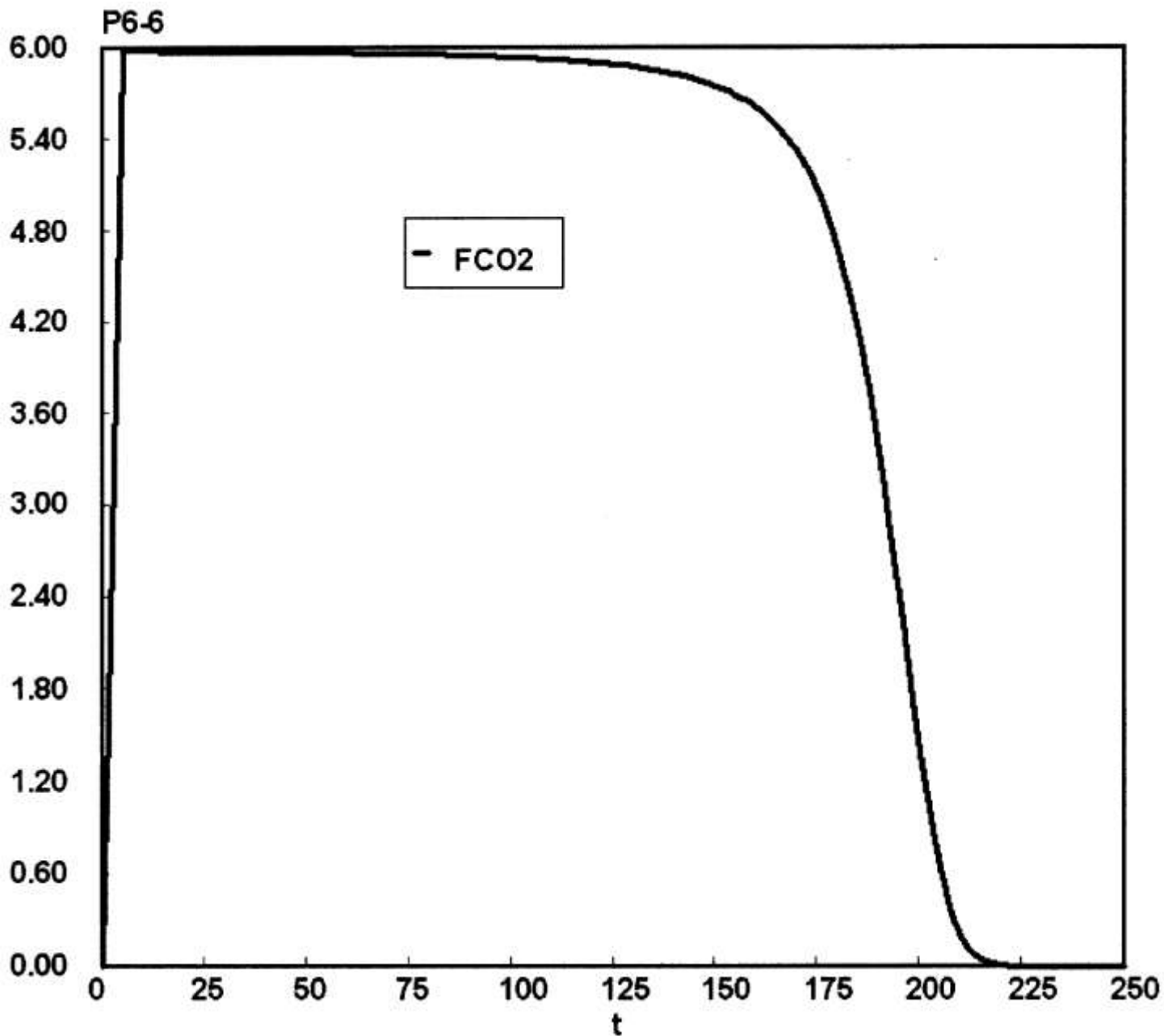
- 1 $C_{b0} = 1.5$
- 2 $F_{b0} = 6$
- 3 $C_{a0} = 0.75$
- 4 $C_c = N_c / V$
- 5 $N_{a0} = 1125$
- 6 $X = (N_{a0} - N_a) / N_{a0}$
- 7 $k = 5.1$
- 8 $\rho = 1000$
- 9 $MW_{CO2} = 44$
- 10 $C_a = N_a / V$
- 11 $C_b = N_b / V$
- 12 $r_a = -k * C_a * C_b$
- 13 $v_o = F_{b0} / C_{b0}$
- 14 $FCO2 = -r_a * V$
- 15 $v_{CO2} = FCO2 * MW_{CO2} / \rho$
- 16 $C_d = C_c$

P6-6 Sembibatch with Moles as the Variable



P6-6 Semibatch with Moles as the Variable





P6-6 Semibatch: Concentrations C_A , C_B , C_C

POLYMATH Report

Ordinary Differential Equations

Calculated values of DEQ variables

| | Variable | Initial value | Minimal value | Maximal value | Final value |
|----|----------|---------------|---------------|---------------|-------------|
| 1 | Ca | 0.75 | 8.846E-14 | 0.75 | 8.846E-14 |
| 2 | Cao | 0.75 | 0.75 | 0.75 | 0.75 |
| 3 | Cb | 0 | 0 | 0.15303 | 0.15303 |
| 4 | Cbo | 1.5 | 1.5 | 1.5 | 1.5 |
| 5 | Cc | 0 | 0 | 0.496826 | 0.45909 |
| 6 | CC | 0 | 0 | 0.496827 | 0.45909 |
| 7 | Cd | 0 | 0 | 0.496827 | 0.45909 |
| 8 | Fbo | 6. | 6. | 6. | 6. |
| 9 | FCO2 | 0 | 0 | 5.987132 | 1.692E-10 |
| 10 | k | 5.1 | 5.1 | 5.1 | 5.1 |
| 11 | MWCO2 | 44. | 44. | 44. | 44. |
| 12 | Na | 1125. | 2.168E-10 | 1125. | 2.168E-10 |
| 13 | Nao | 1125. | 1125. | 1125. | 1125. |
| 14 | NC | 0 | 0 | 1125. | 1125. |
| 15 | Nc | 0 | 0 | 1125. | 1125. |
| 16 | ra | 0 | -0.0039413 | 0 | -6.904E-14 |
| 17 | rate | 0 | 0 | 0.0039413 | 6.904E-14 |
| 18 | rho | 1000. | 1000. | 1000. | 1000. |
| 19 | t | 0 | 0 | 250. | 250. |
| 20 | V | 1500. | 1500. | 2450.5 | 2450.5 |
| 21 | vCO2 | 0 | 0 | 0.2634338 | 7.444E-12 |
| 22 | vo | 4. | 4. | 4. | 4. |
| 23 | Vo | 1500. | 1500. | 1500. | 1500. |
| 24 | X | 0 | 0 | 1. | 1. |

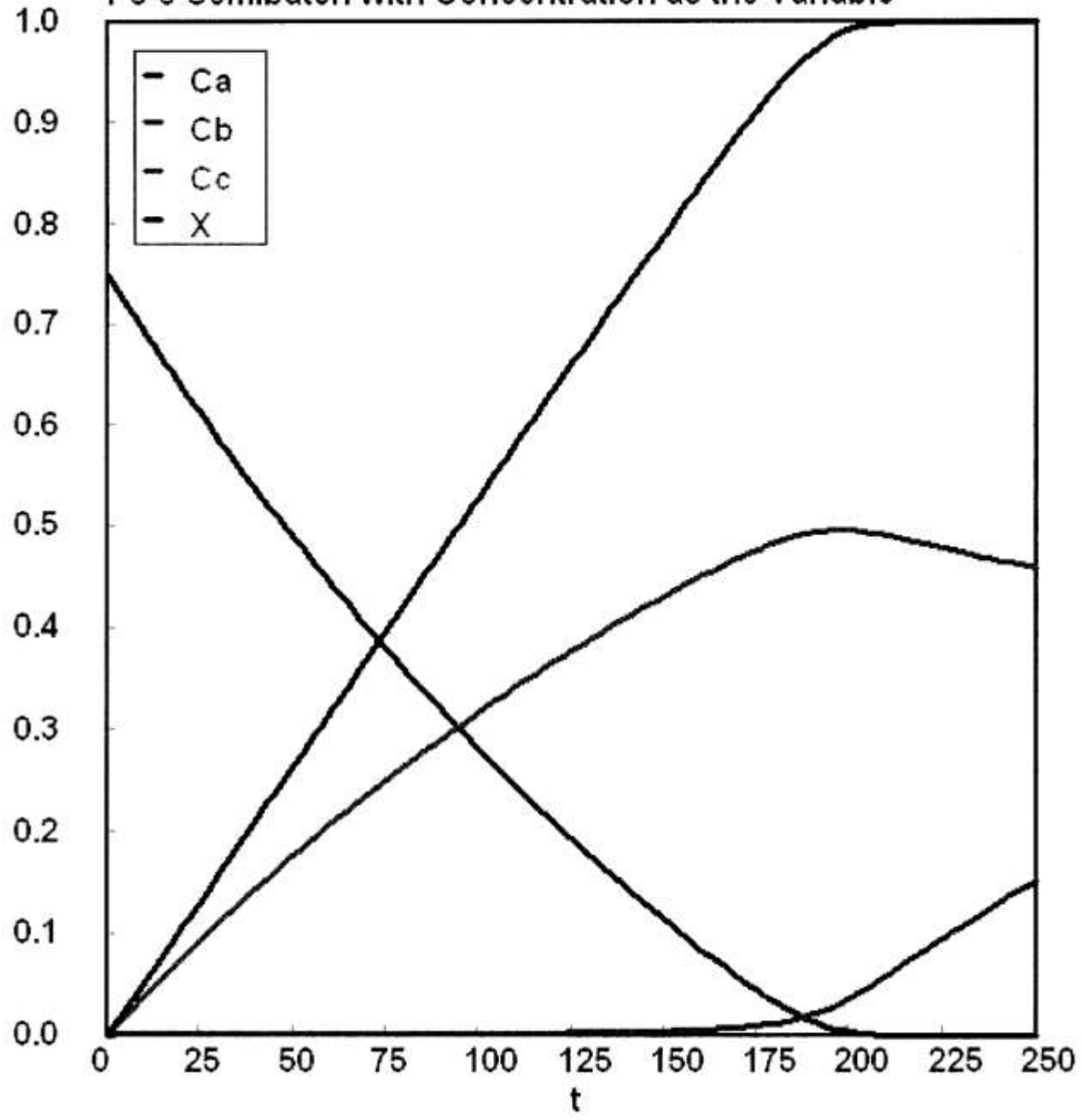
Differential equations

- $d(Ca)/d(t) = ra + ((vo-vCO2) / V) * (-Ca)$
- $d(Cb)/d(t) = ra + vo*Cbo/V + ((vo-vCO2) / V) * (-Cb)$
- $d(Cc)/d(t) = -ra + ((vo-vCO2) / V) * (-Cc)$
- $d(V)/d(t) = vo-vCO2$

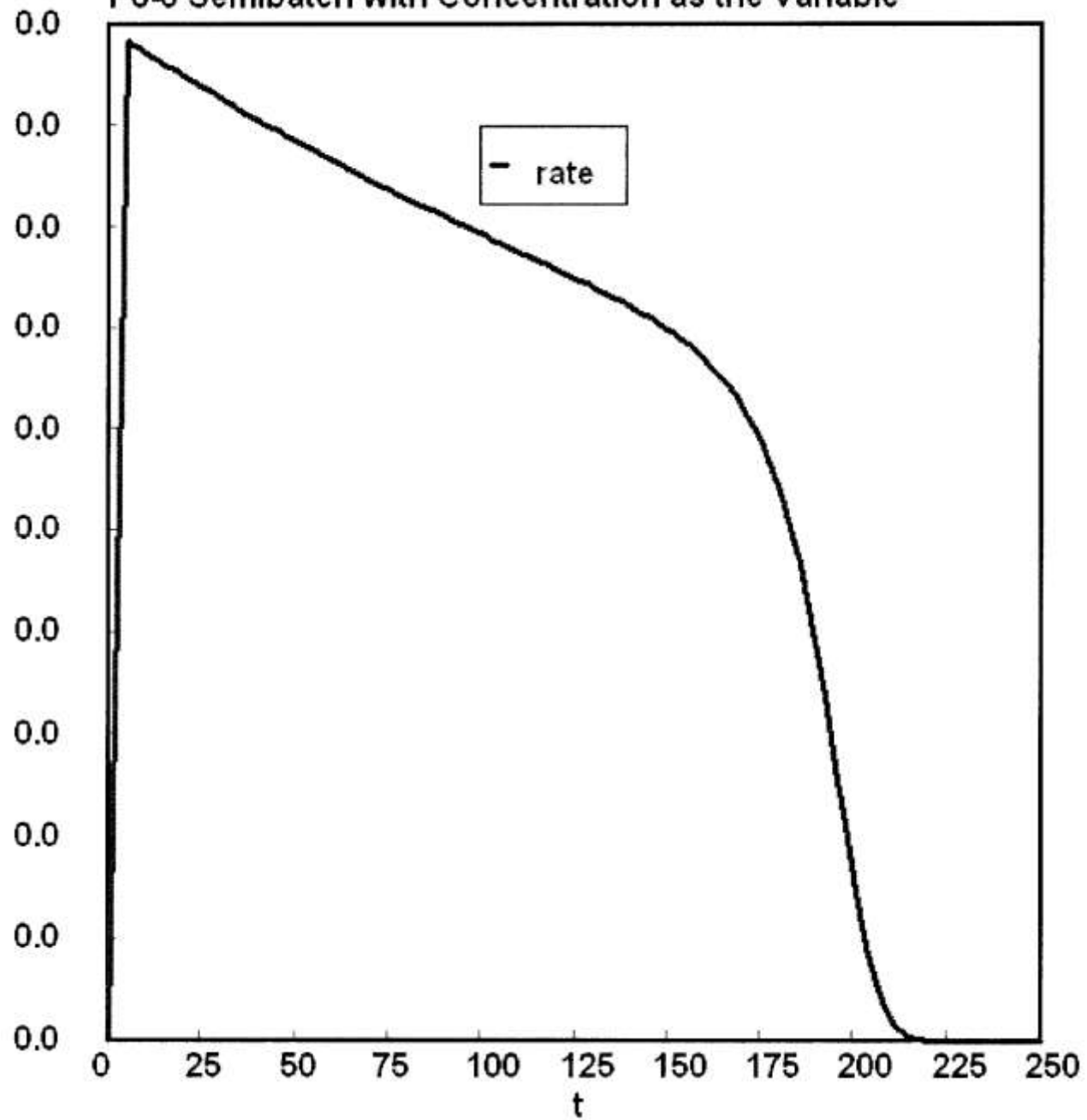
Explicit equations

- $Cd = Cc$
- $Fbo = 6$
- $Cao = 0.75$
- $Vo = 1500$
- $Na = Ca*V$
- $k = 5.1$
- $ra = -k * Ca * Cb$
- $Nao = Cao*Vo$
- $rate = -ra$
- $rho = 1000$
 $rho=1000g \text{ per } dm^3$
- $MWCO2 = 44$
- $FCO2 = -ra*V$
- $NC = Nao - Na$
- $Cbo = 1.5$
- $vo = Fbo / Cbo$
- $vCO2 = MWCO2*FCO2/rho$
- $CC = NC/V$
- $Nc = Cc * V$
- $X = 1 - Ca * V / (Cao*Vo)$

P6-6 Semibatch with Concentration as the Variable



P6-6 Semibatch with Concentration as the Variable



Semibatch Reactors

Three Forms of the **Mole Balances** applied to Semibatch Reactors:

| | | |
|------------------------|--|--|
| 1. Molar Basis | $\frac{dN_A}{dt} = r_A V$ $\frac{dN_B}{dt} = F_{B0} + r_B V$ | |
| 2. Concentration Basis | $\frac{dC_A}{dt} = r_A - C_A \frac{\nu_0}{V}$ $\frac{dC_B}{dt} = r_B + (C_{B0} - C_B) \frac{\nu_0}{V}$ | $\frac{dN_A}{dt} = r_A V$ $\frac{dN_B}{dt} = F_{B0} + r_B V$ |
| 3. Conversion | $\frac{dX}{dt} = \frac{-r_A V}{N_{A0}}$ | |

Semibatch Reactors

Consider the following elementary reaction:



$$-r_A = kC_A C_B$$

The combined **Mole Balance**, **Rate Law**, and **Stoichiometry** may be written in terms of number of moles, conversion, and/or concentration:

| <u>Conversion</u> | <u>Concentration</u> | <u>No. of Moles</u> |
|---|--|------------------------------------|
| $\frac{dX}{dt} = \frac{k(1-X)(N_{B0} + F_{B0}t - N_{A0}X)}{V_0 + v_0t}$ | $\frac{dC_A}{dt} = r_A - C_A \frac{v_0}{V}$ | $\frac{dN_A}{dt} = r_A V$ |
| | $\frac{dC_B}{dt} = r_A + (C_{B0} - C_B) \frac{v_0}{V}$ | $\frac{dN_B}{dt} = F_{A0} + r_B V$ |

Polymath Equations

| <u>Conversion</u> | <u>Concentration</u> | <u>Moles</u> |
|--|--|----------------------------------|
| $d(X)/d(t) = -r_a * V / N_{a0}$ | $d(C_a)/d(t) = r_a - (C_a * v_o) / V$ | $d(N_a)/d(t) = r_a * V$ |
| $r_a = -k * C_a * C_b$ | $d(C_b)/d(t) = r_b + ((C_{b0} - C_b) * v_o) / V$ | $d(N_b)/d(t) = r_b * V + F_{b0}$ |
| $C_a = N_{a0} * (1 - X) / V$ | $r_a = -k * C_a * C_b$ | $r_a = -k * C_a * C_b$ |
| $C_b = (N_{b0} + F_{b0} * t - N_{a0} * X) / V$ | $r_b = r_a$ | $r_b = r_a$ |
| $V = V_0 + v_o * t$ | $V = V_0 + v_o * t$ | $V = V_0 + v_o * t$ |
| $V_0 = 100$ | $V_0 = 100$ | $V_0 = 100$ |
| $v_o = 2$ | $v_o = 2$ | $v_o = 2$ |
| $N_{a0} = 100$ | $F_{b0} = 5$ | $F_{b0} = 5$ |
| $F_{b0} = 5$ | $N_{a0} = 100$ | $C_a = N_a / V$ |
| $N_{b0} = 0$ | $C_{b0} = F_{b0} / v_o$ | $C_b = N_b / V$ |
| $k = 0.1$ | $k = 0.01$ | $k = 0.01$ |
| | $N_a = C_a * V$ | |
| | $X = (N_{a0} - N_a) / N_{a0}$ | |

End of Lecture 10